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OSTEOPOROSIS SCREENING USING RADIOGRAPHIC ABSORPTIOMETRY OF THE MANDIBLE

The present invention relates to preventive medicine and in particular, but not
5 limited, to a method and system using radiographic absorptiometry of the mandible for
osteoporosis screening.

Currently, osteoporosis affects approximately 50 percent of women and 20 percent of
men over the age of 50 in the US. Additionally, osteoporosis occurs sooner if the amount
of bone established at maturity is less than average. Compounding this problem,
10 osteoporosis is typically not discovered early enough for treatment to have the best chance
for success. Until the present invention, routine X-rays have been a poor predictor for
osteoporosis, as prior art methods have only had the ability to show osteopenia once 20 to
30 percent of bone mass is lost, which is considerably late in the course of the disease.

Bone is composed of a mixture of high-turnover trabecular (spongy) bone and slowly
15 changing cortical (compact) bone. Osteoporosis is a bone disease that reduces the amount
of bone. This reduction results in an overall weakening of the affected bones and an
increased risk of hip and vertebral fractures. Such fractures involve considerable
socioeconomic implications in that they cause severe pain, immobility, and often result in
surgery, wherein 25 to 30 percent of patients undergoing hip surgery die within five years
20 of having this operation.

Bone mineral density (BMD) is a useful predictor of bone strength and indirectly of
fracture risk. Bone mineral density is usually reported as the standard deviation compared
to either peak bone mass (T-score) or compared to age matched controls (Z-score). The
World Health Organization defines osteopenia as bone mass that is from -1 to -2.5

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standard deviations (S.D.) of peak bone mass and osteoporosis as bone mass that is below
-2.5 standard deviations of peak bone mass. Typically, in clinical practice, bone mineral
densitometry is performed at target sites such as the lumbar spine (L1-L4) and the hip
(femoral neck), which are sites particularly susceptible to osteoporotic fractures. At those
5 target sites, bone mineral densitometry provides a measure of the amount of bone and thus
an indication of whether the patient is suffering from osteoporosis, since in osteoporosis
there is a proportional loss of both matrix and material. As a rule of thumb, the fracture
risk is doubled for each standard deviation below the peak bone mass. This increases
exponentially, so the fracture risk is four times greater at -2 S.D. and eight times greater at
10 -3 S.D.

Currently, dual energy X-ray absorptiometry (DXA) and quantitative computed
tomography (QCT) are the BMD tests of choice for diagnosing osteoporosis. Although
the availability of DXA and QCT devices has increased over the last decade, only a small
percentage of the population undergoes BMD testing to facilitate early detection of
15 osteoporosis. The associated expense (e.g., equipment cost, dedicated space, and
personnel) is a major reason for the lack of BMD testing. Another is the inconvenience of
its use as a preventive medicine tool, which requires a separate appointment and trip to a
testing facility. Additionally, DXA and QCT testing must follow complex protocols,
which are poorly reproduced in a community setting. Accordingly, there is a need for an
20 inexpensive screening method for osteoporosis that may be performed easily and routinely
for the overall benefit of the patient and society.

The present invention is a method and apparatus providing for the inexpensive
screening for osteoporosis using conventional dental X-ray equipment. Dentists are

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currently the only healthcare providers whom patients regularly see, even if they are not ill, making the dental office environment an ideal mass-screening setting for osteoporosis. Additionally, the wide availability of dental X-ray equipment as well as its initial low cost and low cost of use creates an inexpensive screening method for osteoporosis, which may
5 be performed easily and routinely for the overall benefit of the patient and society.

The inventors have conducted a pilot study designed to 1) evaluate the range of mandible size, density and homogeneity in the general population and 2) assess a custom calibration wedge as a means of normalizing radiographs for varying exposure and film development conditions. The X-ray exposure parameters were maintained constant for all
10 subjects. Periapical radiographs of a selected region of interest, such as the posterior mandible, and a calibration element were simultaneously acquired under single-energy and dual-energy conditions.

The patients of the pilot study group fell into the following categories: I (female, age 25-35), II (male, age 25-35), III (female, age 50+), IV (male, age 60+) and V (persons at
15 high risk for osteoporosis). Using the device of the present invention, a significant difference in mandibular BMD between Categories III and V ($p=0.1$) was detected. Additionally, mandibular BMDs were positively correlated with a body mass index ($R=0.55$, $p=0.005$) and shown to decrease with age. Furthermore, as BMD decreased, increased variance within the regions of interests (ROIs) was observed. A typical number
20 for correlation of bone mineral density at different sites in the body (e.g., lumbar vertebrae and hip, hip and radius) is about 0.7. The values obtained by the present invention in the selected ROIs have been similarly correlated with the spine and hip, confirming that the

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selected ROIs of the pilot study meet the criteria of having a large percentage of trabecular bone.

The benefits of the present invention are the opportunistic screening in a setting where equipment exists and people visit, an optimized dual-energy measurement that
5 reduces inaccuracies due to soft tissue effects, and a well-calibrated measurement. This information can be used by a physician to diagnose osteoporosis and recommend treatment strategies.

In one aspect of the present invention provided is a method to screen for osteoporosis damage to a patient's bones. The method comprises placing in the mouth of the patient
10 adjacent to a mandibular bone being tested, a dental radiographic absorptiometric device comprising at least one calibration element. X-ray energy is applied to the dental radiographic absorptiometric device simultaneously through the mandibular bone and the calibration element to generate both a bone absorptive record from the mandibular bone and a calibration element absorptive record from the calibration element. The bone
15 absorptive record is analyzed against the calibration element absorptive record to determine the extent, if any, of the osteoporosis damage to the mandibular bone.

In another aspect of the invention provided is one embodiment of a dental radiographic absorptiometric device adapted for osteoporosis screening using a standard dental X-ray machine and being locatable in a patient's mouth. The device comprises an
20 image portion having a first surface, and a biting block portion attached to the first surface of the image portion. The biting block portion defines a cavity, and at least one calibration element is accommodated in the cavity of the biting block portion.

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Further provided is another embodiment of a dental radiographic absorptiometric device adapted for osteoporosis screening using a standard dental X-ray machine and being locatable in a patient's mouth. The device comprises an image portion having a first surface, and a biting block portion attached to the first surface of the image portion. The biting block portion defines a cavity, and at least one calibration element and at least one of an upper beam filter are accommodated in the cavity of the biting block portion. The device also includes at least one of a lower beam filter provided to the imaging portion below the biting block portion.

These and other features and objects of the present invention will be apparent in light of the description of the invention embodied herein.

The following detailed description of the embodiments of the present invention can be best understood when read in conjunction with the following drawings, where like structure is indicated with like reference numerals and in which:

FIGS. 1A is a front illustration view, partially cutaway, of the non-digital embodiment of a dental radiographic absorptiometric device according to the present invention;

FIG. 1B is a side illustration view of the non-digital embodiment of FIG. 1A;

FIG. 1C are illustrations of calibration wedge arrangements suitable for use with the embodiment of FIG. 1A;

FIG. 2 is an illustration of the non-digital device according to the present invention situated in the mouth of a patient and being radiated by X-rays from a conventional dental X-ray machine;

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FIG. 3 shows an X-ray image in accordance with the present invention showing calibration data, filtered bone mineral density readings, and a predetermined region of interest; and,

FIGS. 4A and 4B are front and side illustration views, respectively, of a digital
5 embodiment of a dental radiographic absorptiometric device according to the present invention;

The present invention provides an opportunistic approach to osteoporosis screening at the time of routine check-ups in the dental health care setting using radiographic absorptiometry. In particular, radiographic absorptiometric measurements of the mandible
10 are taken using a dental radiographic absorptiometric device to determine the amount or net bone structure inside the bone that an X-ray beam from a standard dental X-ray machine penetrates. The present invention may be applied to either non-digital or digital radiographic absorptiometry.

Referring to FIGS. 1A and 1B, illustrated are front and side views, respectively, of a
15 non-digital embodiment of a dental radiographic absorptiometric device 10 according to the present invention. The non-digital device 10 is adapted to take periapical radiographs of a patient. In the illustrated embodiment, the non-digital device 10 is generally rectangular and may be provided in a number of sizes to easily fit in an adult mouth. The non-digital device 10 comprises a biting portion 12 to allow the patient to bite down so
20 motion is less problematic, and an imaging portion 14. The biting portion 12 includes, generally shown, a calibration element 13, which includes a upper beam filter 16a and a calibration wedge 18. The device 10 further includes a lower beam filter 16b provided to image portion 14 below the biting portion 12. The beam filters 16a and 16b are optimized

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in material and thickness to provide, in combination with the calibration wedge 18, a radiographic image of the mandible that permits early evaluation of a patient for osteoporosis.

Although the non-digital device 10, the beam filters 16a and 16b, and the calibration
5 wedge 18 are all illustrated as rectangular, other geometric shapes may be used.

Furthermore, although the illustrated non-digital device 10 is configured for a dual-energy measurement, as will be explained hereafter, the non-digital device is suitable for a single-energy measurement using calibration wedge 18 with or without beam filters 16a and/or 16b.

10 The biting portion 12 of the non-digital device 10 is a relatively thick rectangular structure and is either integral with the imaging portion 14, or mounts thereon. The imaging portion 14 is a relatively thin rectangular structure comprising a base layer 15 and a removable cover layer 17. The base layer 15 is in the path of the X-rays and adds to the X-ray attenuation. The cover layer 17 is removably attached to the base layer 15 to
15 provide an enclosure for accommodating a standard periapical radiographic film 20. The biting portion 12 and imaging portion 14 are made of polycarbonate, plastic, acrylic, methyl methacrylate, any other suitable low attenuating materials, and combinations thereof.

The beam filters 16a and 16b are provided in upper and lower portions of device 10
20 to spectrally filter the output of the X-ray source into two distinct X-ray spectra and to provide an optimized dual-energy measurement, which reduces inaccuracies due to soft tissue effects. As illustrated, the upper beam filter 16a is provided in front of the calibration wedge 18. Alternatively, the upper beam filters 16a may be provided behind

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the calibration wedge 18, if desired. The upper beam filter 16a comprises a first pair of filters 11a and 11b. In the lower portion of device 10, the lower beam filter 16b comprises a second pair of filter 11a and 11b, which substantially span the width of the imaging portion 14 in a side-by-side orientation. These first and second pairs of filters 11a and 11b
5 simultaneously yield adjacent higher and lower energy images in both upper and lower portions of film 20 for comparative assessment of relative optical densities.

Filters 11a and 11b are each a thin sheet material having a thickness of about 0.05 mm to about 0.12 mm. In particular, filters 11a and 11b each comprises a material selected from cerium, molybdenum, any other suitable material, and combinations thereof. In one
10 specific embodiment, the first filter 11a is 0.075 mm Ce and the second filter 11b is 0.10 mm Mo; however, in other embodiments varying number of suitable filters with varying thicknesses and similar atomic numbers may be used. It is to be appreciated that the thickness of filter materials is dependant on atomic number, kilo-voltage settings of the dental X-ray machine, and the desired filtration factor. For example, a dental X-ray
15 machine setting in the range from about 60 kVp to about 80 kVp is suitable for taking mandible measurements using the above-mentioned beam filter thicknesses and materials. If desired, the non-digital device 10 may be conveniently configured to permit the exchanging of beam filters of various thicknesses and materials, which is generally illustrated by a side-to-side arrow, such as for example, via slots 19 provided in the device
20 10.

In the illustrated embodiment of FIGS. 1A and 1B, the calibration wedge 18 is provided in a cavity 24 of the biting portion 12, and is situated adjacent to the base layer 15 of the imaging portion 14. The calibration wedge 18 is made of copper, its alloys, and

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any other suitable material and provides a series and/or gradient of incrementally changing contrast test objects. In this manner, with each exposure of the non-digital device 10, the calibration wedge 18 provides calibration data to film 20.

In one embodiment, the calibration wedge 18 is a step wedge, or alternatively, a
5 smooth tapered wedge, such as wedge 21d. In the illustrated embodiment, seven-steps are used, which changes the image contrast by approximately 14.3% per step. If desired, finer or coarser contrast increments may be provided with more or fewer steps, respectively. In particular, the calibration wedge 18 has dimensions of about 3mm by about 25mm and has steps of thicknesses ranging from about .05 mm to .33 mm. In other embodiments, the
10 wedge dimension and step thicknesses may vary somewhat and still provide sufficient contrast to calibrate the resulting image on film 20.

If desired, a set of wedges 21 may be used to provide high and low energy calibration references, in which a number of such calibration arrangements are illustrated by FIG. 1C. In one embodiment, the set of wedges 21 comprises overlaying wedge 18 with another
15 wedge 21a in a crisscross arrangement. In another embodiment, the set of wedges 21 comprise a calibration wedge 21b provided adjacently to another calibration wedge 21c in a side-by-side orientation. In still another embodiment, the set of wedges 21 comprises a calibration wedge 21d provided adjacently to another calibration wedge 21e in a counter side-by-side orientation. The wedges may be a smooth (tapered) or step wedge.
20 Additionally, in the embodiments using the set of wedges 21, one wedge may comprise acrylic for a soft tissue reference, and the other wedge may comprise copper or aluminum for a bone tissue reference. The set of wedges 21 can similarly be inserted into cavity 24 of the biting portion 12, if so used.

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The calibration wedge 18 provides a "gray scale" image of objects with known absorption differences, which allows the image analysis system to analyze the exposed film. It is to be appreciated that the calibration of individual films is very important.

5 Variability in acquisition parameters can significantly affect the measured values. When radiographic exposures are made, the X-ray tube settings, patient size and patient composition (lean mass vs. fat) play a role in the resultant lightness or darkness of the film. Further, film development, chemical age and temperature affect film intensity values. Therefore, each film is normalized against a standard provided by the calibration
10 wedge 18 in order to adjust for differences among X-ray equipments, exposures, types of film, and the development process. Additionally, the calibration wedge 18 can be used as part of a quality control procedure to evaluate the dental equipment at each screening site.

The film 20 has an optical density that varies systematically, e.g., logarithmically, in accordance with the amount of radiation exposure. To increase its efficiency and lower
15 the required dosage of X-rays, the film 20 optionally can be sandwiched between sheets of plastic called intensifying screens 22. Each intensifying screen 22 is a plastic base coated with an X-ray sensitive phosphor and which converts X-rays into light to produce the latent image on the film 20.

Referring to FIG. 2, the non-digital device 10 is conveniently used with traditional
20 dental radiography. In one embodiment, osteoporosis screening is performed by imaging the mandible using standard dental X-ray equipment and standard dental film. Since osteoporosis is a generalized disease, its effects are not limited to the spine and hip. Since

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osteoporotic bone loss is mainly a result of hormonal changes, it has been found that osteoporotic patients show bone loss also in the mandible.

In operation, the non-digital device 10 is introduced at the proper location within the patient's mouth 26, and the patient is instructed to bite down on the biting portion 12
5 between corresponding upper and lower teeth 28 and 30. Ideally, a perpendicular orientation between a X-ray position indicating device (or simply "cone") 32 and the non-digital device 10 will be maintained with respect to a line of sight 34 for X-rays emanating from the cone 32 to eliminate distortions, improper focus and the like. If desired, an aiming device (not shown) provided to cone 32 can conveniently be used with the non-
10 digital device 10 of the present invention.

The biting portion 12 is dimensioned to fit in between the upper and lower teeth 28 and 30, such that the patient may close his or her mouth. Optionally, however, the biting portion 12 may be sized to extend outwardly from the patient's mouth such that the cheek and/or lips 31 of the patient do not come between the X-ray source, the calibration element
15 13, and the portion of the film 20 situated behind the calibration element. By this arrangement, a portion of the film is unaffected by the soft tissue effect and provides an accurate normalized reference for each exposure.

When X-rays pass through the patient's mouth 26 during a dental exam, more X-rays are absorbed by the denser parts (such as teeth and bone) than by soft tissues (such as
20 cheeks and gums) before striking film 20, and creating an image thereon. As illustrated by FIG. 3, which is an example of a mandibular radiographic image according to the present invention, the molars of the lower teeth 30 will appear lighter because fewer X-rays penetrate to reach the film 20. The calibration element 13 provided above the teeth and

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gums will appear to have a varying degree of darkness because each progressive rectangular portion of the calibration wedge 18 permits more X-ray penetration. The calibration element 13 is therefore used for determining energy distribution and attenuation coefficients.

5 In one embodiment, the mandible is used as the bone measurement site. In another embodiment, the trabecular bone in the area between the roots of the second bicuspid and the first molar and from the superior border of the mandible to approximately one-half of the molar root length is designated as the region of interest (RIO) 29 for these measurements. Other ROIs between other teeth or roots also may be selected and
10 advantageously used with the present invention. In particular, analysis locations could be chosen where the variance of optical density values could be related to the progression of bone loss.

After imaging using a low x-ray dose, the resulting image 23 on film 20 is subsequently analyzed for optical values (e.g., pixel grayscale values) relating to
15 calibration and bone equivalent densities. This analysis can be automated by digitizing the image 23 on the film 20 with a film digitizer. The resulting optical values extracted by the film digitizer can then be analyzed using an algorithm that subtracts the soft-tissue effects from the digitized images and compares the intensities of the bone and the calibration wedge at specific locations to determine bone density and bone mineral content. The
20 result of this analysis may be used to classify a patient's BMD as either "normal" or "below normal" at the specific bone measurement site locations, which can be used as a recommendation to seek further diagnosis or treatment.

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In a dual-energy embodiment, calibration values are extracted from an upper portion 23a of the resulting image 23. As illustrated, the upper portion 23a is divided into upper and lower regions 25a and 25b, which corresponds to the portions of the film 20 located behind the first (upper) pair of filters 11a and 11b and calibration wedge 18. As with the upper portion 23a, the lower portion 23b of the resulting image 23 is divided into upper and lower regions 27a and 27b, which corresponds to the portions of the film 20 located behind the second (lower) pair of filters 11a and 11b. Since the beam filters 16a and 16b are same in both the biting and imaging portions 12 and 14 of the device 10, the upper region 27a of the lower portion 23b is exposed to the same energy level as the upper region 25a of the upper portion 23a during imaging. Likewise, the lower region 27b of the lower portion 23b is exposed to the same energy level as the lower region 25b on the upper portion 23a. In this manner, dual-energy images and calibration data is provided concurrently on film 20.

Hard tissue mass is determined from the dual-energy images and calibration data provided on film 20. At a point on the high-energy calibration wedge image where the optical density is identical to that of the high-energy mandible image, the following equation applies:

$$e^{-\mu_{WH}(E)d_W} = e^{-(\mu_{SH}(E)d_S + \mu_{BH}(E)d_B)}$$

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A second similar equation can be created with the corresponding low-energy data:

$$e^{-\mu_{WL}(E)d_W} = e^{-(\mu_{SL}(E)d_S + \mu_{BL}(E)d_B)}$$

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where d_W is the wedge thickness, d_S is the soft tissue thickness, d_B is the bone thickness, and μ_W , μ_S , and μ_B are the energy-dependent linear attenuation coefficients for the wedge material(s), soft tissue and bone, respectively. The subscripts L and H refer to low-energy and high-energy values. Since the wedge thickness at each step is known and attenuation coefficient values for the wedge material(s), bone and soft tissue are available in the literature, the only unknowns are the bone and soft tissue thicknesses d_B and d_S , which are easily solved using conventional techniques. Of course, although only specific wedge optical density values corresponding to the individual steps are available from the image data, the wedge-equivalent thickness for any optical density may be found using appropriate interpolation techniques.

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As previously mentioned, device 10 can be provided with or without beam filters 16a and/or 16b and used with a single-energy. In such a single-energy embodiment, the pixel values in the region of interest are extracted and averaged. The resulting average value is then compared to a calibration curve generated from extracted calibration wedge values from the image 23 on film 20 to yield an equivalency density value. For example, a young person might have an equivalent bone mineral density in the mandible of 240 microns of copper whereas an osteoporotic patient's value might be equivalent to 100 microns of copper.

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It is to be appreciated that the disclosed pilot study mentioned in the summary of the invention validated the device 10 using a single-energy and the disclosed thickness range of the copper step wedge. In particular, patient bone mineral densities (BMDs) were
5 assessed using a film algorithm, which correlated optical density (OD) to BMD determinations in mandibular measurements from the selected region-of-interest 29 (FIG. 3). Based on over 100 irradiations, dozens of calibration curves were developed and incorporated in the film algorithm. It is envisioned that further data will be obtained from a large, population-based study for determining the distribution of mandibular bone
10 mineral density values, expressed in units of copper-equivalency, for all types of patient classifications.

The present invention also includes an automated image analysis process that outlines the regions of interest and teeth. Such an embodiment is comprised of an image digitization component and an automated image analysis component. Radiographs of the
15 mandible and the calibration wedges are acquired and digitized following the above-mentioned procedure. As illustrated also by FIG. 3, teeth 30, bone and soft tissue 38, and a region of interest 29 are outlined on a digitized image of the film 20 by the image analysis component, which then provides computed density values of each of these regions relative to the density of the calibration wedge.

20 Referring to FIGS. 4A and 4B, illustrated are front and side views, respectively, of a digital embodiment of a dental radiographic absorptiometric device 39 according to the present invention. In a digital radiography embodiment, the dental film 20 (FIG. 1B) is replaced with digital sensors 40. After each exposure, an image is provided on a computer

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screen. The images are conveniently stored in computer memory, from which they can be easily retrieved, combined, and manipulated to supply more information. The chemical waste associated with film processing is eliminated, and most significantly, patients are exposed to much less of the X-ray dosage typically delivered in the non-digital

5 embodiment.

It is to be appreciated that the primary difference between digital radiographic absorptiometry (DRA) and its non-digital predecessor is that the image capture, display and analysis functions are performed by one system at a physician's site, without the use of X-ray film. In the DRA embodiment, calibration wedges 18 and beam filters 16 are still
10 used in conjunction with the biting portion 12. The digital sensor 40 may comprise a phosphor screen 42 and a charge-coupled device (CCD) camera 44, CMOS wafers, or any other suitable electronic sensor. As with the non-digital device 10, the digital device 39 is placed in the patient's mouth and irradiated by the X-ray source. Visible photons emitted from the phosphor screen 42 are collected and imaged by the charge-coupled device
15 camera 44. The camera's digital output, via a wire 46, is sent to a PC, which analyzes the image for bone density and bone mineral content in real-time using the same above-mentioned optical scanning techniques.

While the invention has been particularly shown and described with reference to the preferred embodiments thereof, it will be understood by those skilled in the art that various
20 changes in form and details may be made without departing from the spirit and scope of the invention.